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=====
TEXSTAN(academic)
s10.dat, lam, Blasius, Ts(x)
stepsize: constant, dx= .100
entrainment based only on mom + energy eqns;   enfra= 1.00E-06   fra= .010
dpdx: not-a-knot spline curve fit
energy eqn: solved, no source terms
kfluid= 1 const props
  po= 1.01325E+05   den= 1.17700E+00   vis= 1.83800E-05   sp_ht= 1.00500E+03
  prc(je)= .707
initial profiles: kstart= 4   dyi= 5.000E-05   rate= .0900
laminar flow at xstart, transition not possible
axx= 0.0000E+00   bxx= 0.0000E+00   cxx= 0.0000E+00   dxx= 0.0000E+00
exx= 0.0000E+00   fxx= 0.0000E+00   gxx= 0.0000E+00
Stanton number and htc based on (ts-tinf)
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Laminar flat plate flow benchmark
cf/2,theo = 0.332/sqrt(rex)
nux,theo = 0.332*(rex**0.5)*(pr(je,np1)**0.33)
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intg	rex	rem	cf2	nu	cfrat	nurat	h12	reh
5	1.008E+03	2.108E+01	1.046E-02	9.4	1.000	.995	2.590	2.598E+01
100	2.180E+03	3.103E+01	7.110E-03	13.8	1.000	.995	2.590	3.846E+01
200	5.074E+03	4.735E+01	4.658E-03	21.0	.999	.993	2.590	5.893E+01
300	9.175E+03	6.367E+01	3.464E-03	28.2	.999	.993	2.590	7.940E+01
400	1.448E+04	7.999E+01	2.757E-03	35.4	.999	.993	2.590	9.985E+01
500	2.100E+04	9.632E+01	2.290E-03	42.6	1.000	.992	2.590	1.203E+02
600	2.873E+04	1.126E+02	1.958E-03	49.8	1.000	.992	2.590	1.407E+02
700	3.766E+04	1.290E+02	1.710E-03	57.0	1.000	.992	2.590	1.612E+02
800	4.780E+04	1.453E+02	1.518E-03	64.2	1.000	.992	2.590	1.816E+02
900	5.916E+04	1.616E+02	1.365E-03	71.4	1.000	.992	2.590	2.020E+02
1000	7.172E+04	1.779E+02	1.239E-03	78.7	1.000	.992	2.590	2.225E+02
1100	8.549E+04	1.943E+02	1.135E-03	85.9	1.000	.992	2.590	2.429E+02
1200	1.004E+05	2.105E+02	1.048E-03	93.1	1.000	.992	2.590	2.632E+02
1300	1.165E+05	2.268E+02	9.724E-04	100.3	1.000	.992	2.590	2.836E+02
1400	1.339E+05	2.431E+02	9.071E-04	107.5	1.000	.992	2.590	3.041E+02
1500	1.524E+05	2.594E+02	8.504E-04	114.7	1.000	.992	2.590	3.244E+02
1600	1.722E+05	2.757E+02	8.000E-04	121.9	1.000	.992	2.590	3.448E+02
1695	1.921E+05	2.912E+02	7.574E-04	128.7	1.000	.992	2.590	3.642E+02